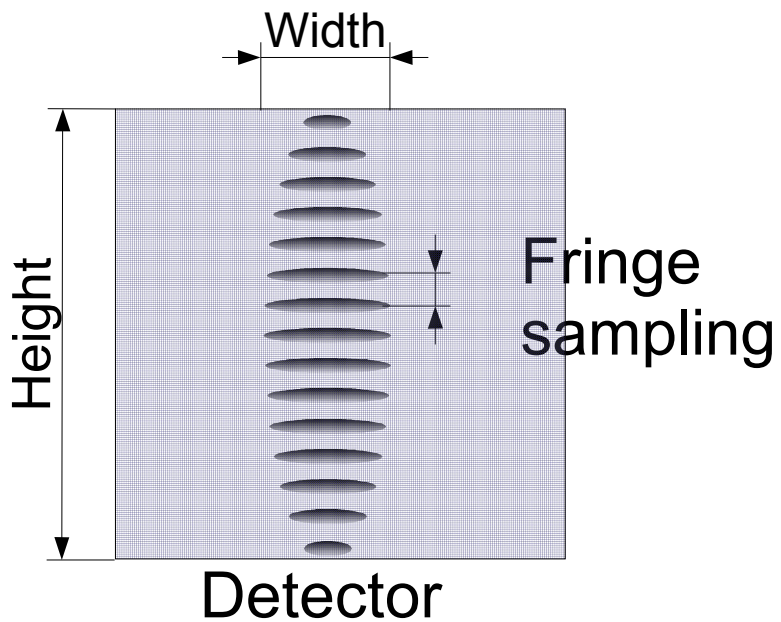
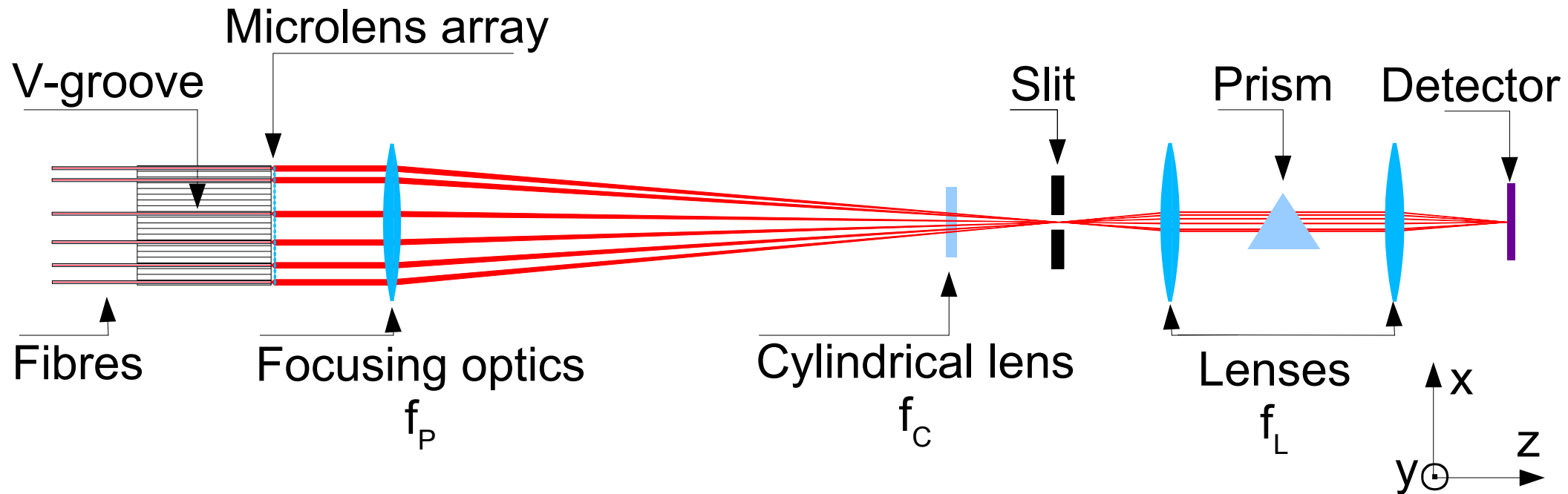


Overview of MIRC spectrograph



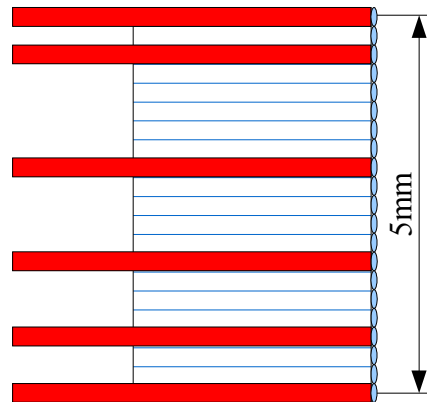
- Fringe sampling:
 - fibers spacing
 - pixel size
 - f_P
- Image Width/Height ratio:
 - f_C

Fringe sampling - 1

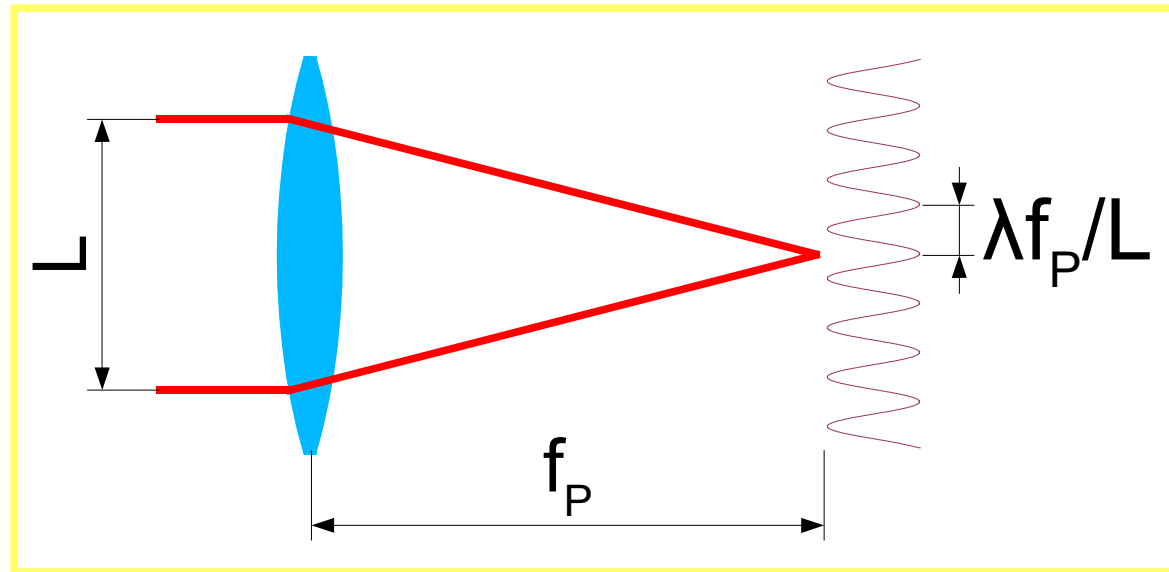
- Minimum requirement (Nyquist): 2px/fringe
- Chosen sampling: 2.5px/fringe @1.5 μ m

- Detector = PICNIC chip
- Pixel size = 40 μ m x 40 μ m

- Fibers spacing: two main configurations:
 - 6 telescopes: 2-6-5-4-3
 - 4 telescopes: 2-6-4



Fringe sampling - 2



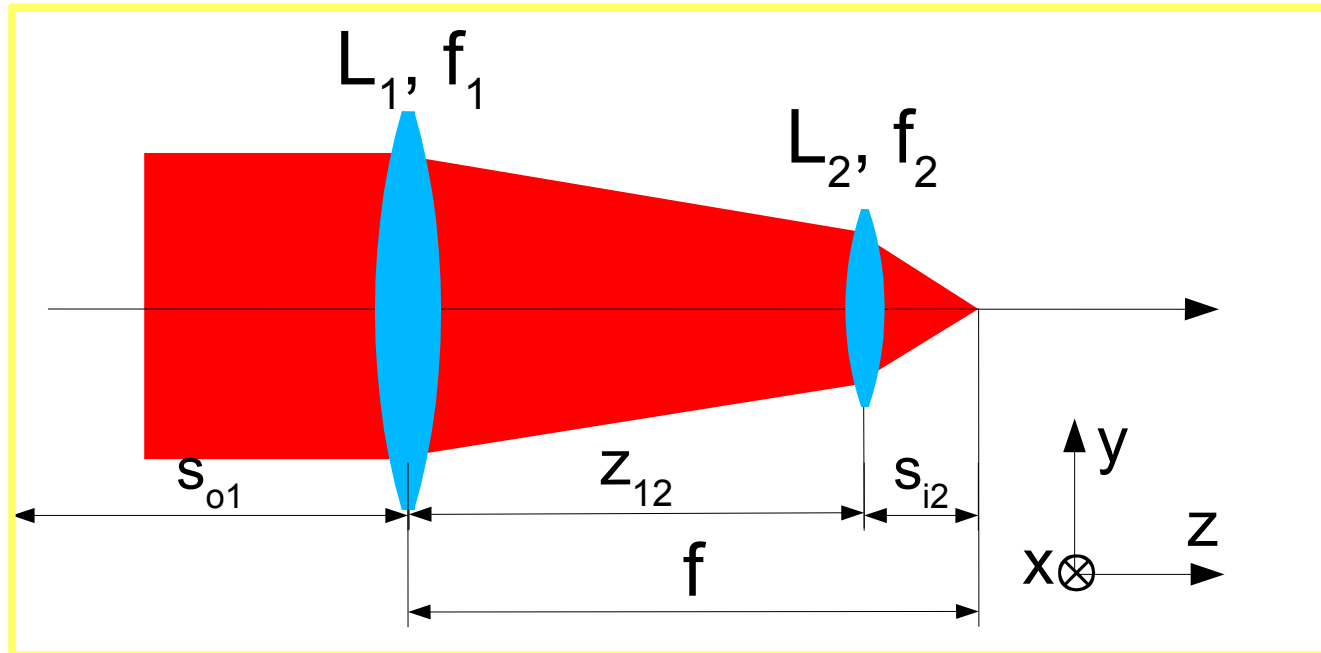
2.5px/fringe @ 1.5 μ m

$$\rightarrow \lambda f_p / L = 2.5 \times p$$

$$\rightarrow f_p = 2.5 \times p \times L / \lambda$$

- 6 telescopes:
 - $f_p = 2.5 \times 40\text{e-}3 \times 5 / 1.5\text{e-}3 = 333\text{mm}$
- 4 telescopes:
 - $f_p = 2.5 \times 40\text{e-}3 \times 3 / 1.5\text{e-}3 = 200\text{mm}$

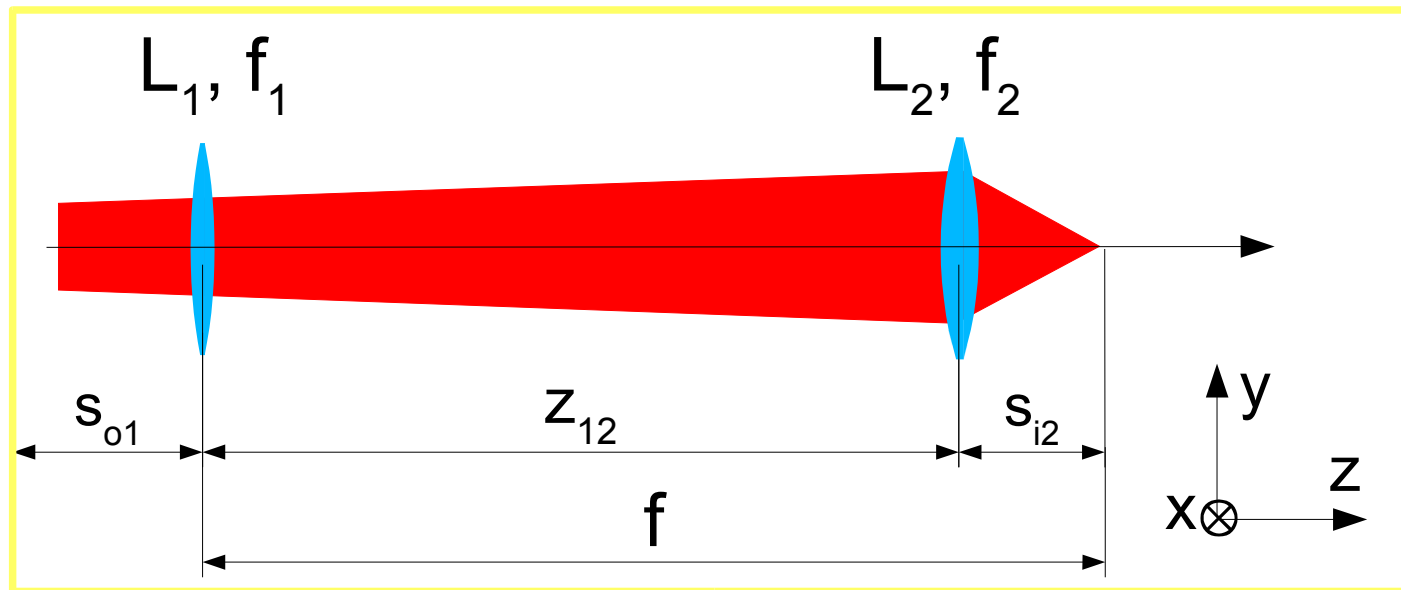
Lens combination – Geometrical Optics



$$s_{i2} = \frac{(z_{12} - f_1) f_2}{z_{12} - f_1 - f_2}$$

$$f_1 = 333\text{mm}, f_2 = 20\text{mm}, z_{12} = 312\text{mm} \\ \Rightarrow s_{i2} = 10.2\text{mm}$$

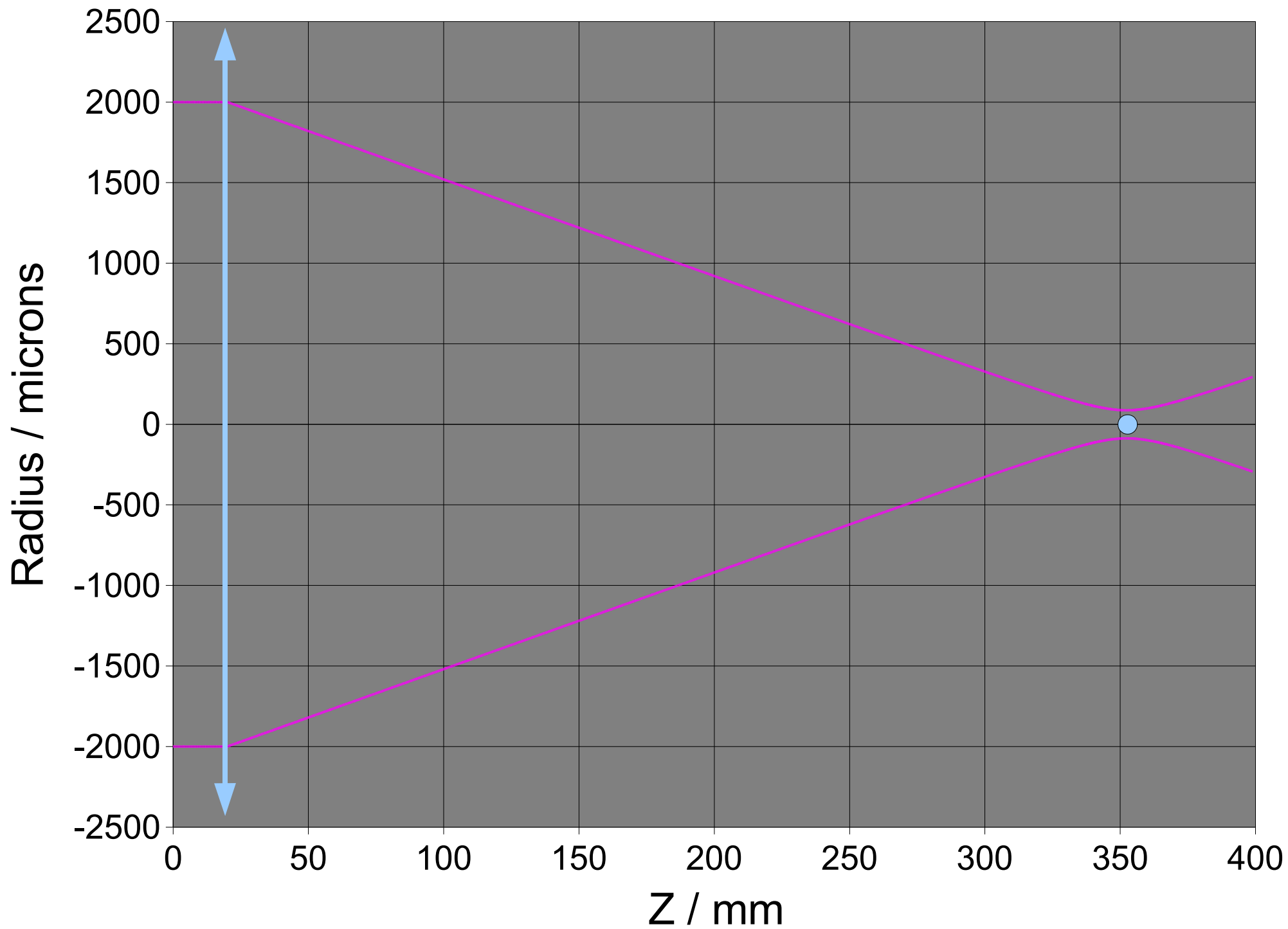
Lens combination and Fresnel diffraction

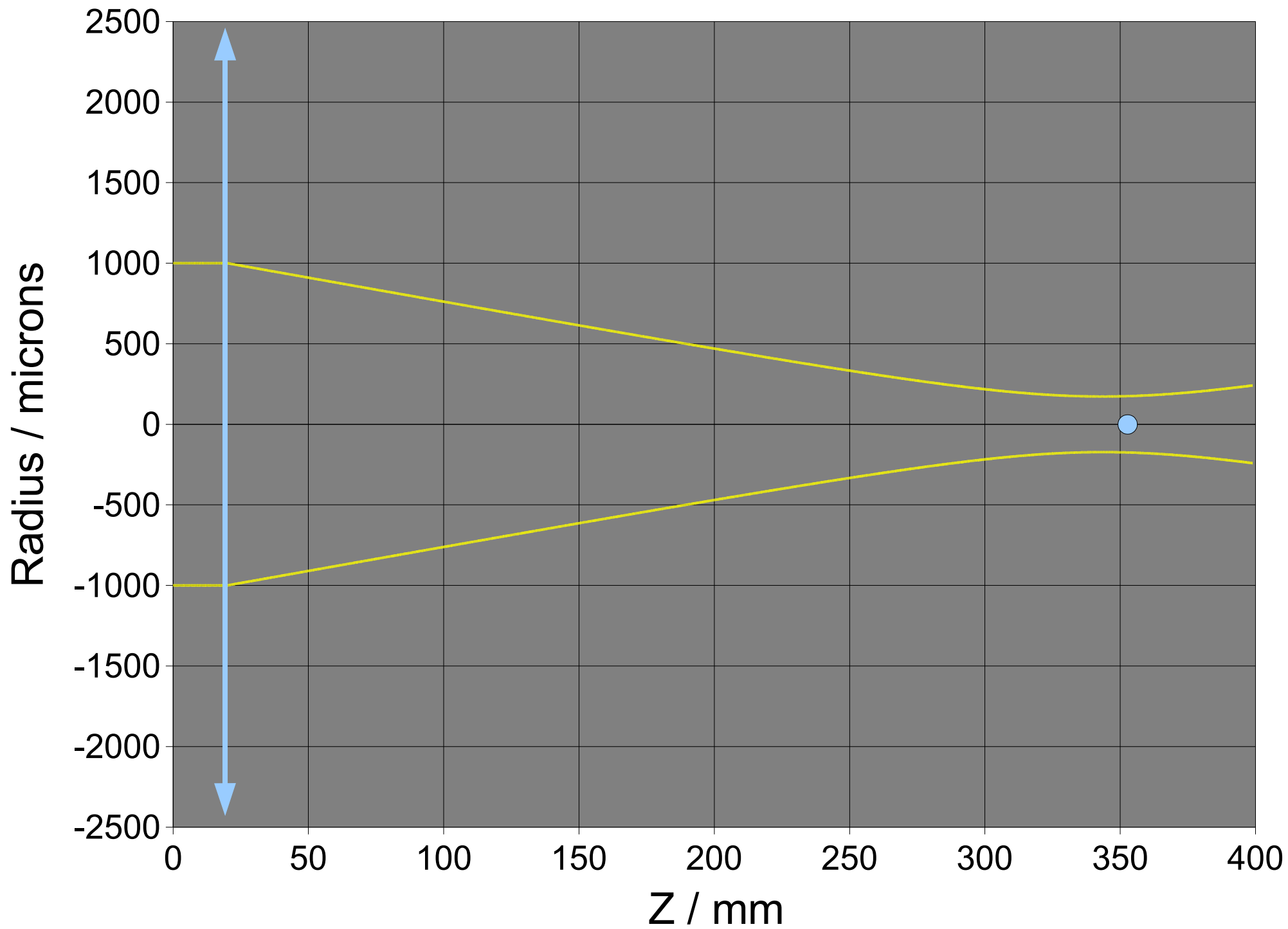


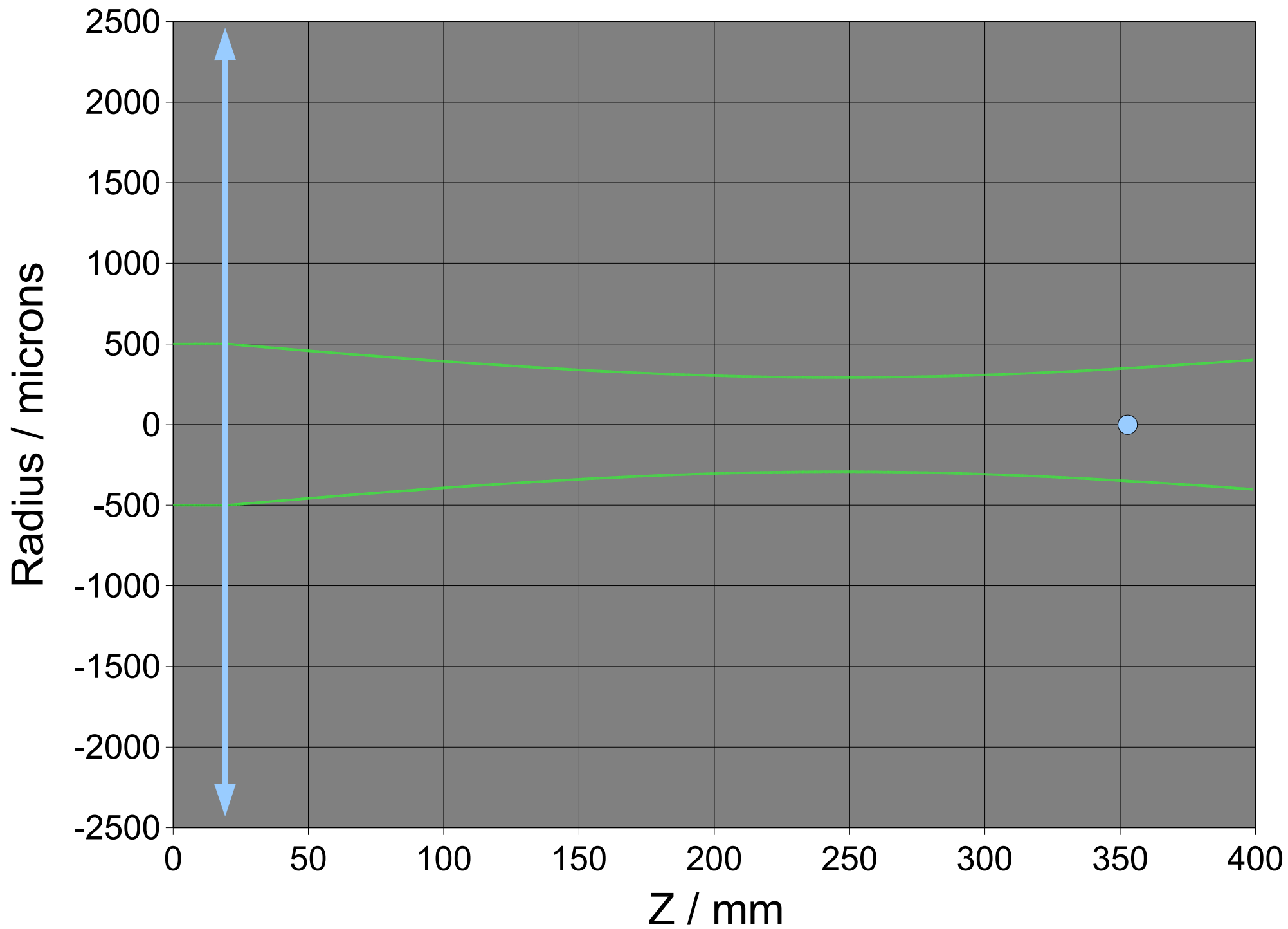
- Beam diameter $\ll s_{o1}, f_1, z_{12}$
- f_1 long focal length == low power
- Fresnel diffraction $\gg f_1$ power

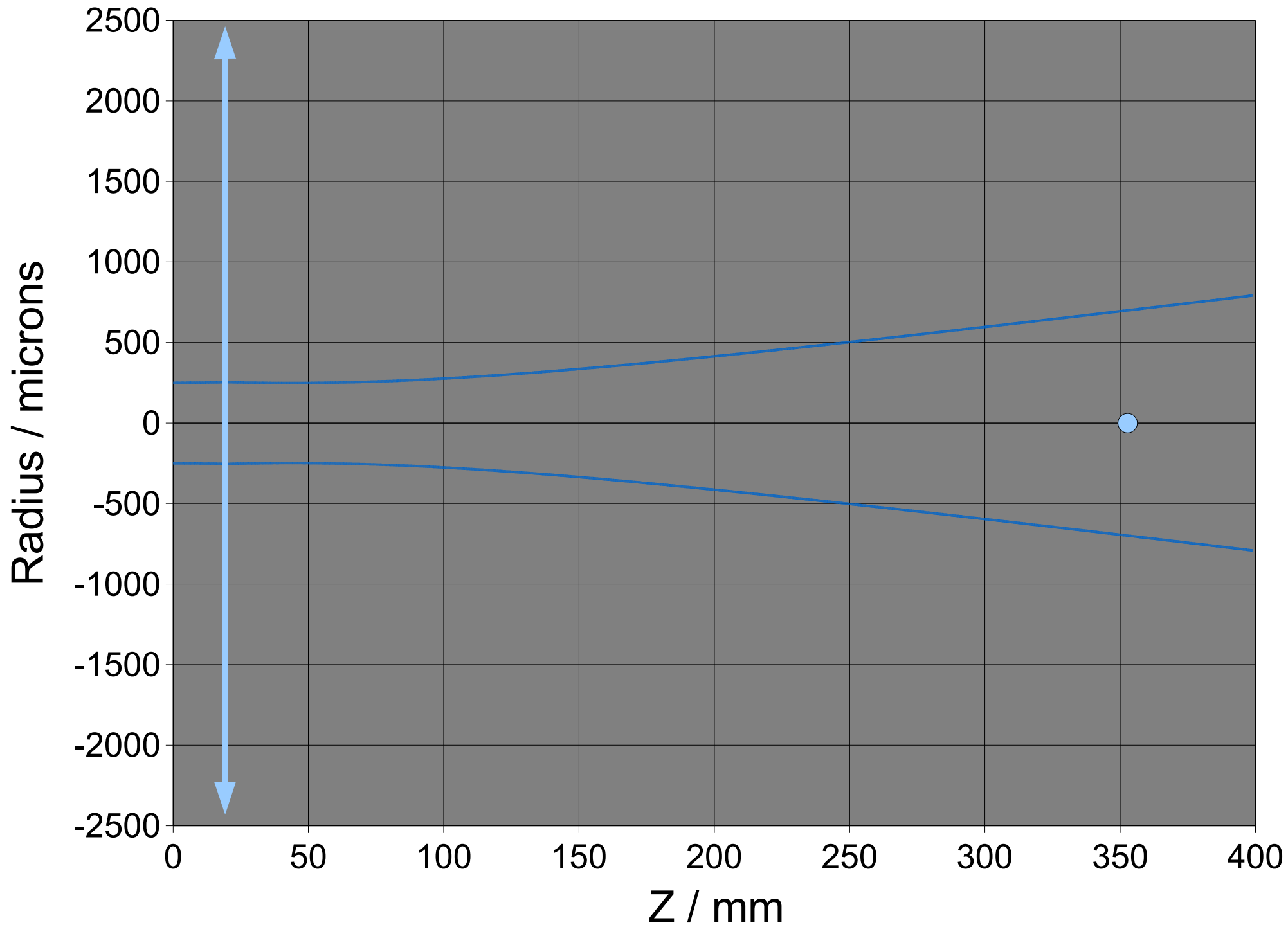
$$s_{i2} = \frac{(z_{12} \cdot f_2)}{z_{12} - f_2} = \text{thin lens equation with } s_o = z_{12}$$

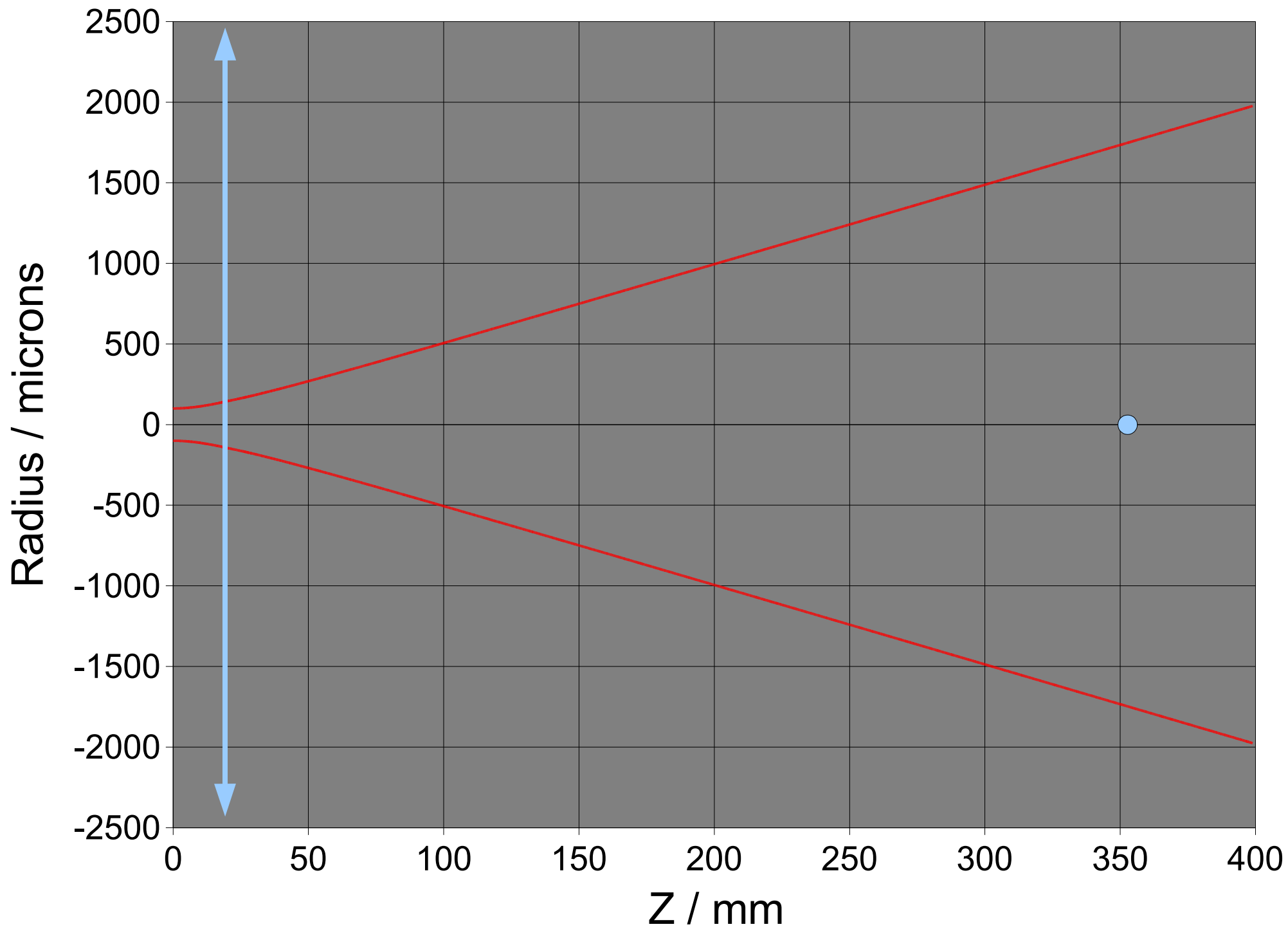
$$f_2 = 20\text{mm}, z_{12} = 312\text{mm} \\ \Rightarrow s_{i2} = 21.4\text{mm}$$



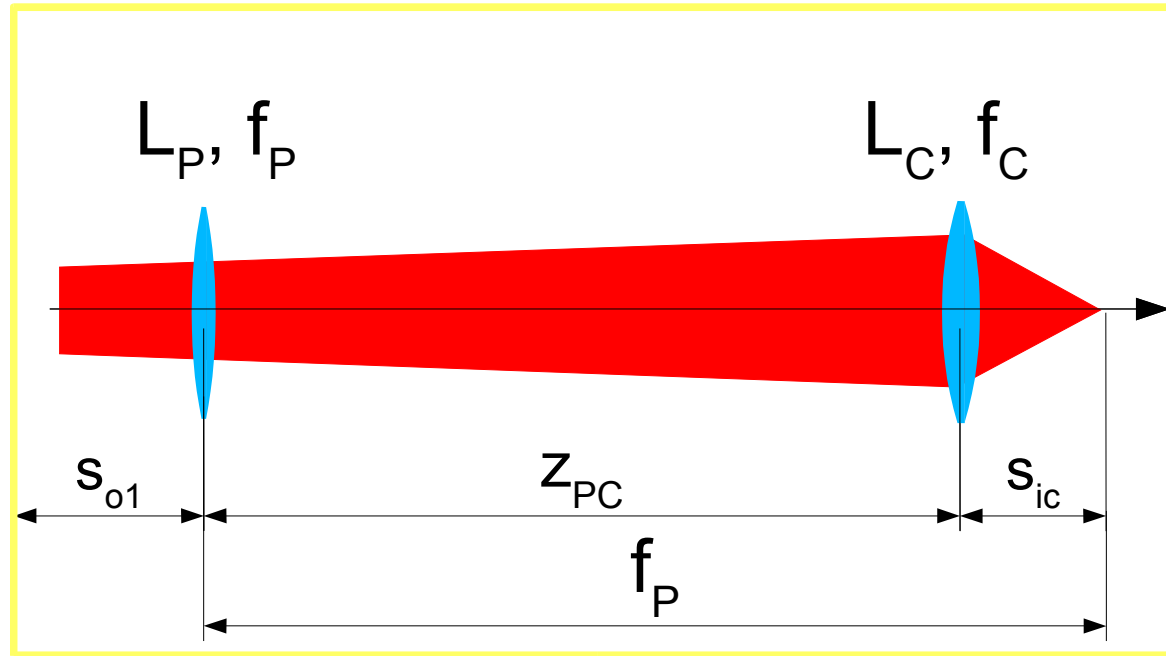








The Cylindrical Lens



$$s_{ic} \approx \frac{z_{PC} \cdot f_C}{z_{PC} - f_C}$$

with $z_{PC} + s_{ic} = f_P$

$$\Rightarrow z_{PC}^2 - f_P z_{PC} + f_P f_C = 0$$

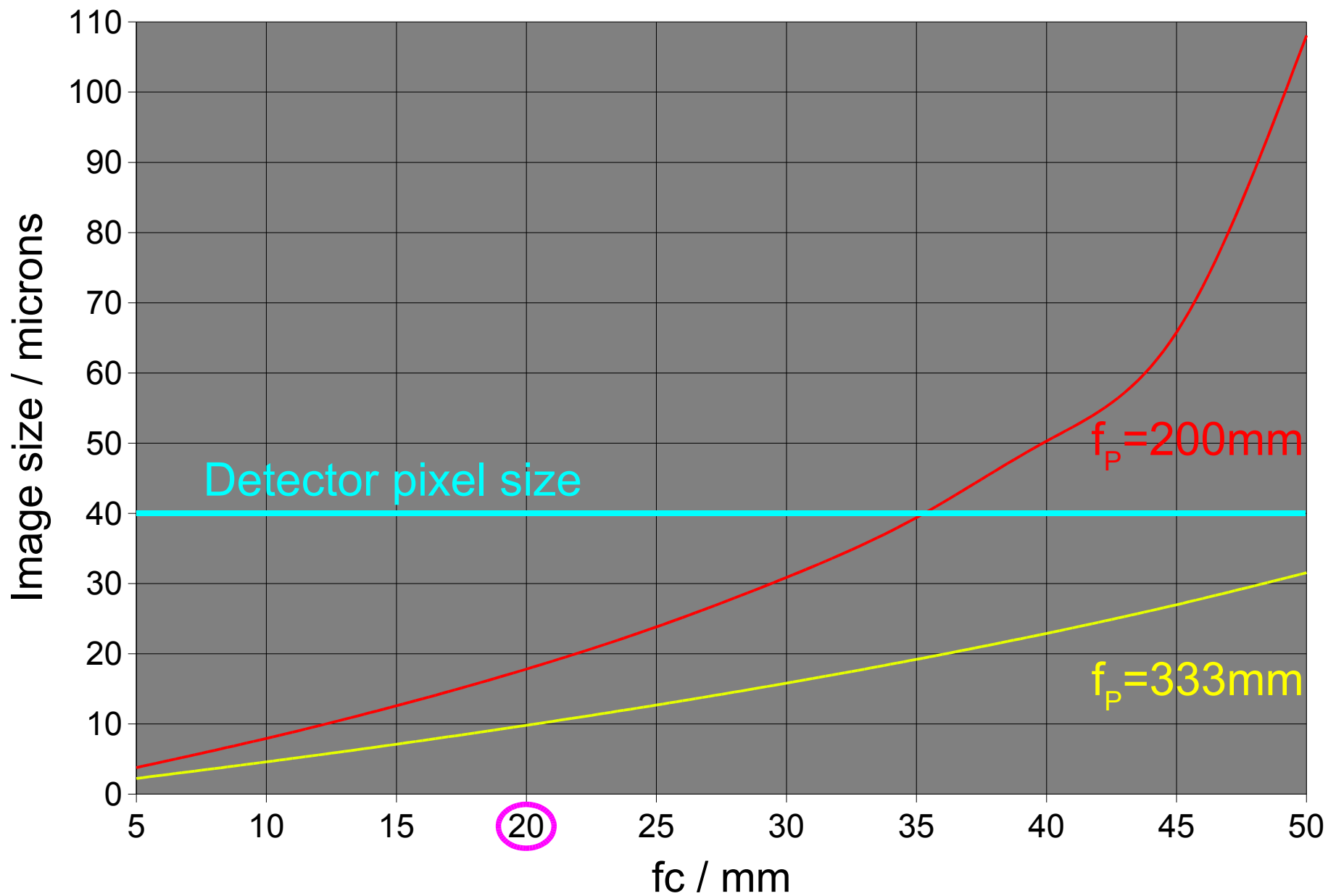
$$f_C \leq \frac{f_P}{4}$$

$$z_{PC} = \frac{f_P + \sqrt{f_P^2 - 4f_P f_C}}{2}$$

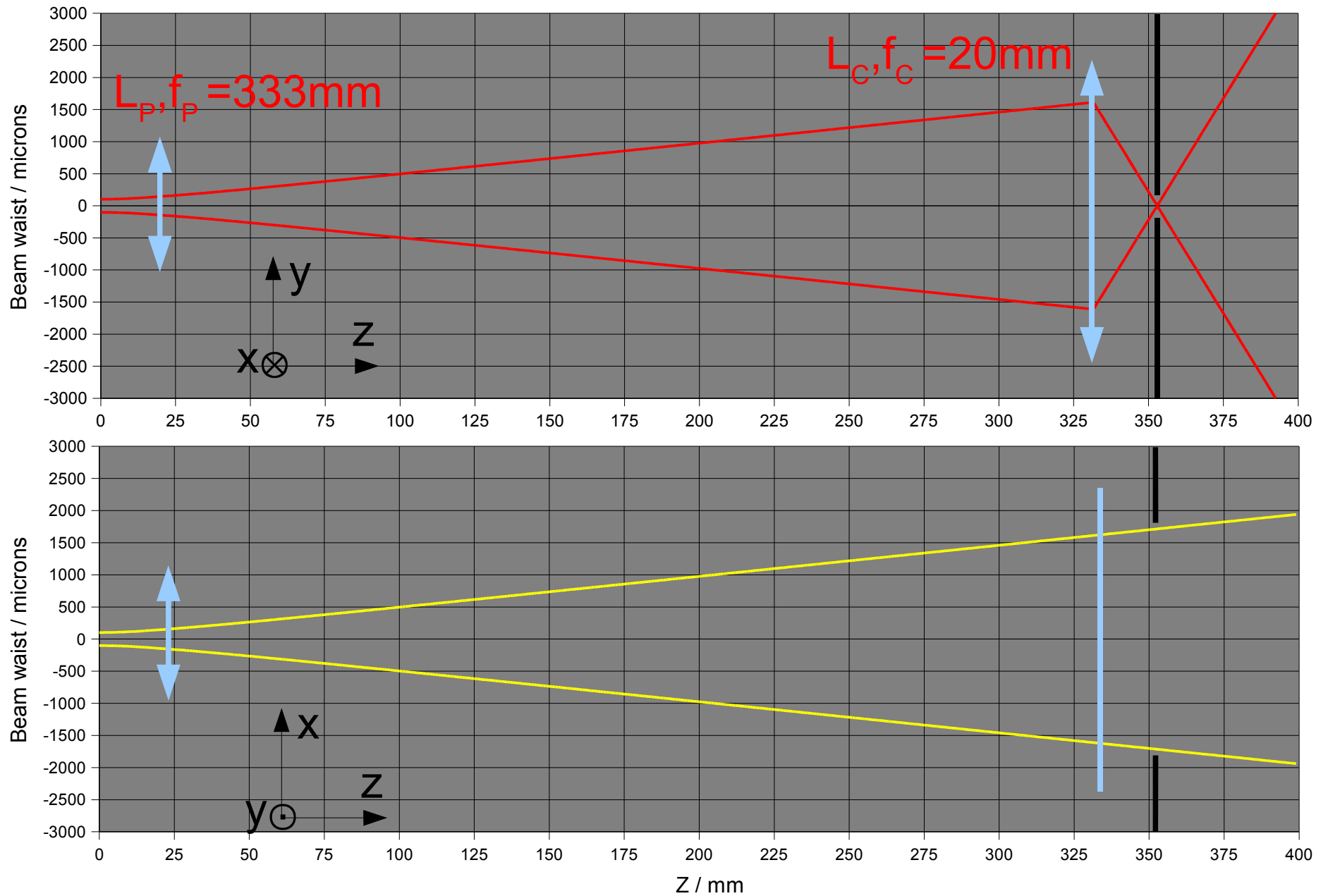
$$f_P = 200 \text{ mm} \rightarrow f_C \leq 50 \text{ mm}$$

$$f_P = 333 \text{ mm} \rightarrow f_C \leq 83 \text{ mm}$$

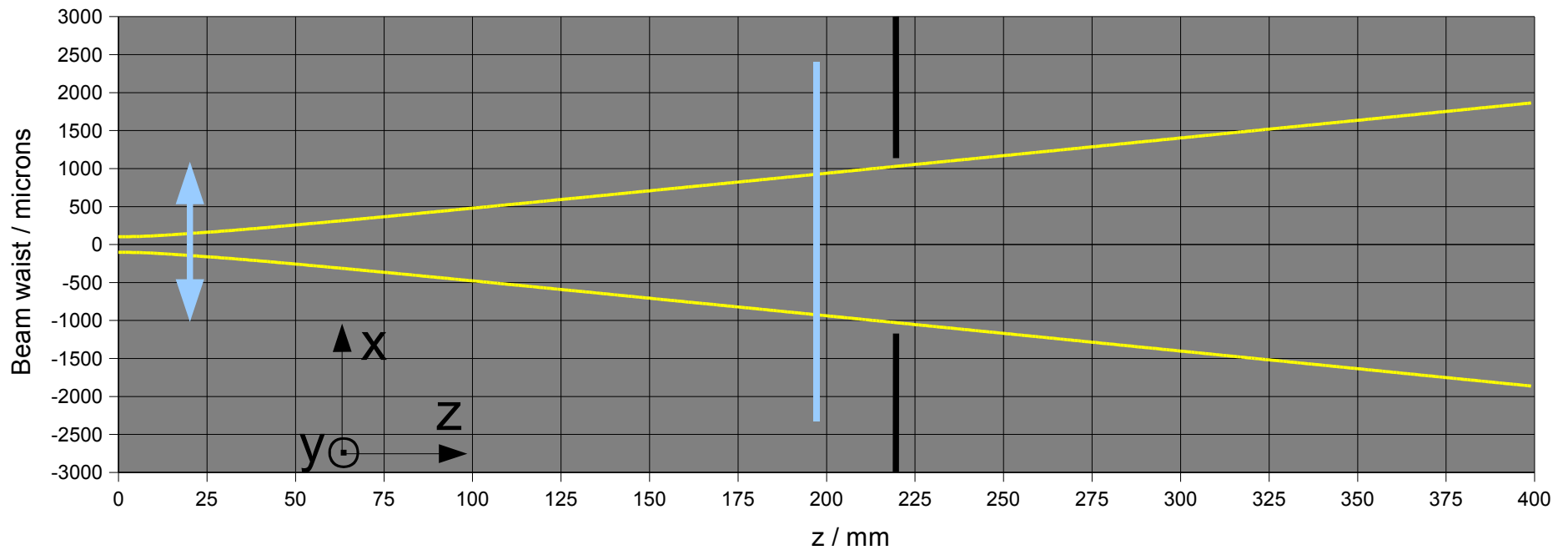
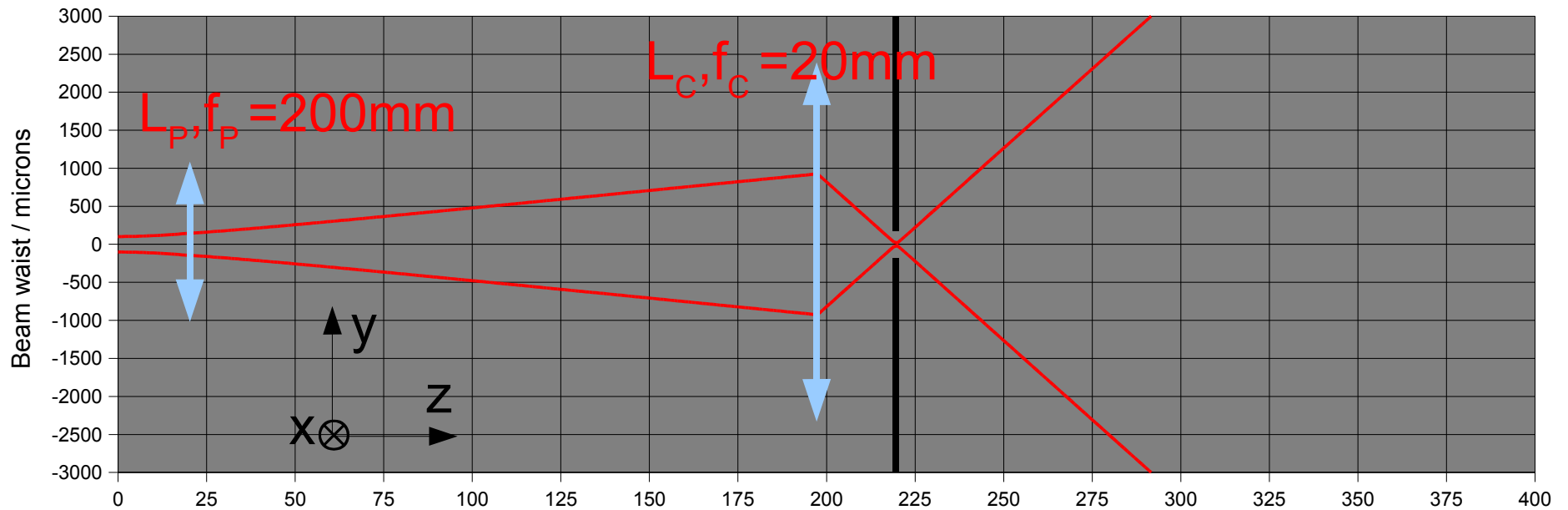
The Cylindrical Lens



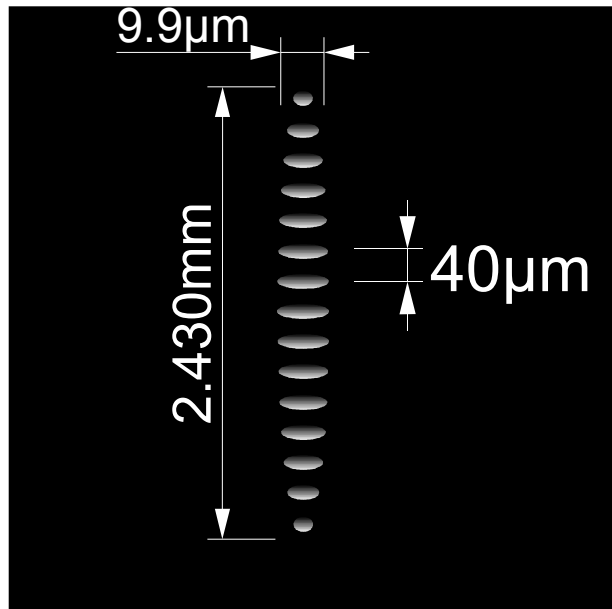
Diffracted beam profile



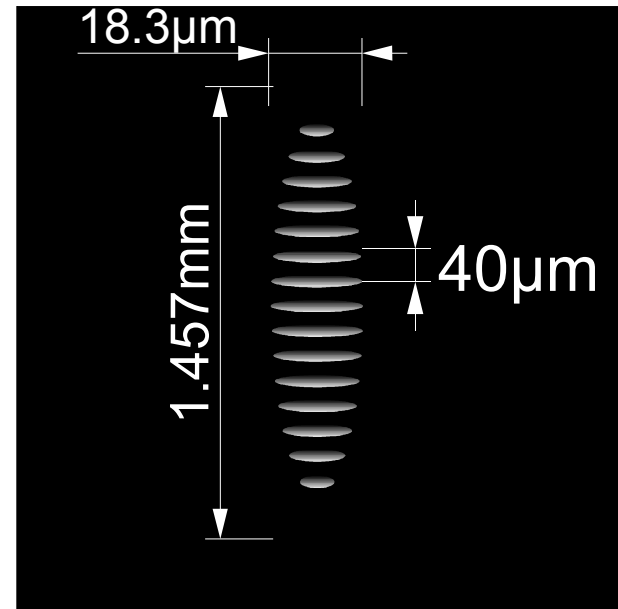
Diffracted beam profile



Images in L_p focal plane

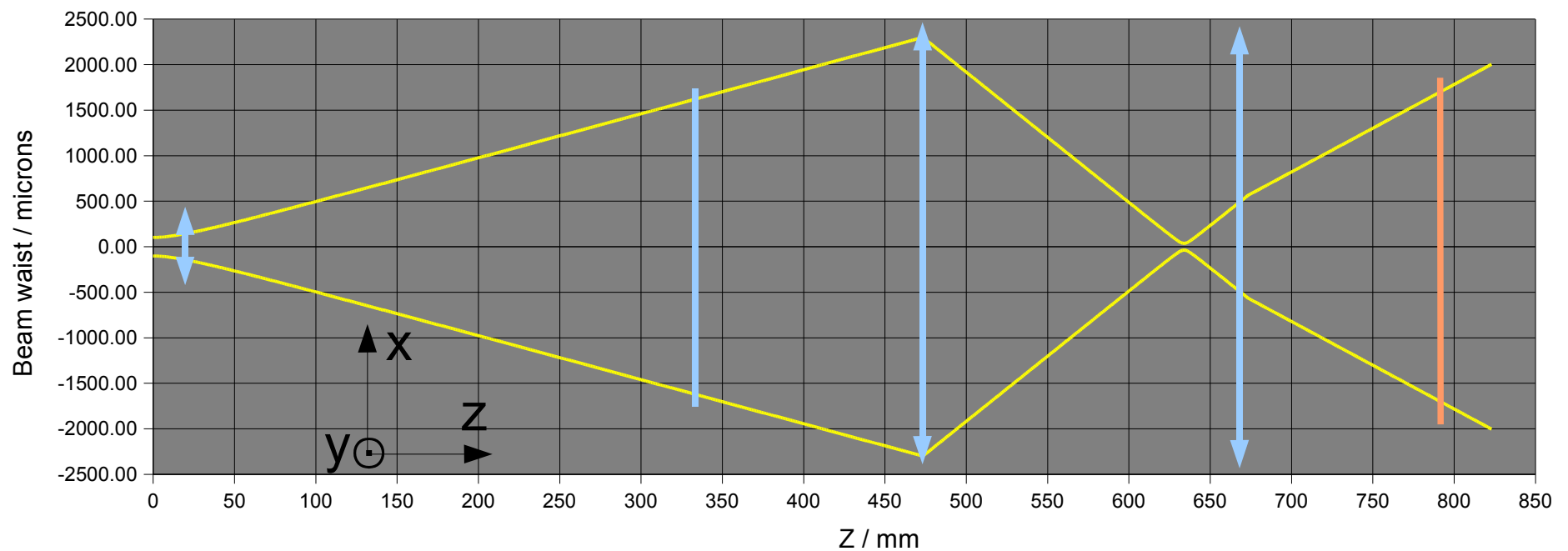
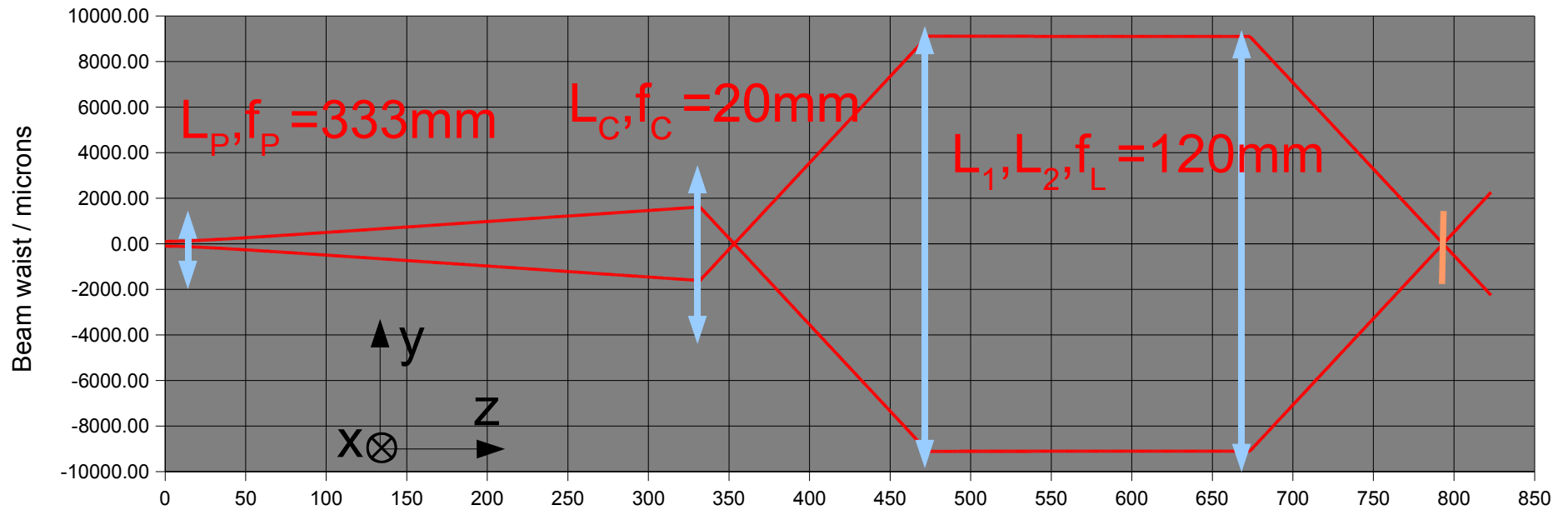


$f_p = 333\text{mm}$

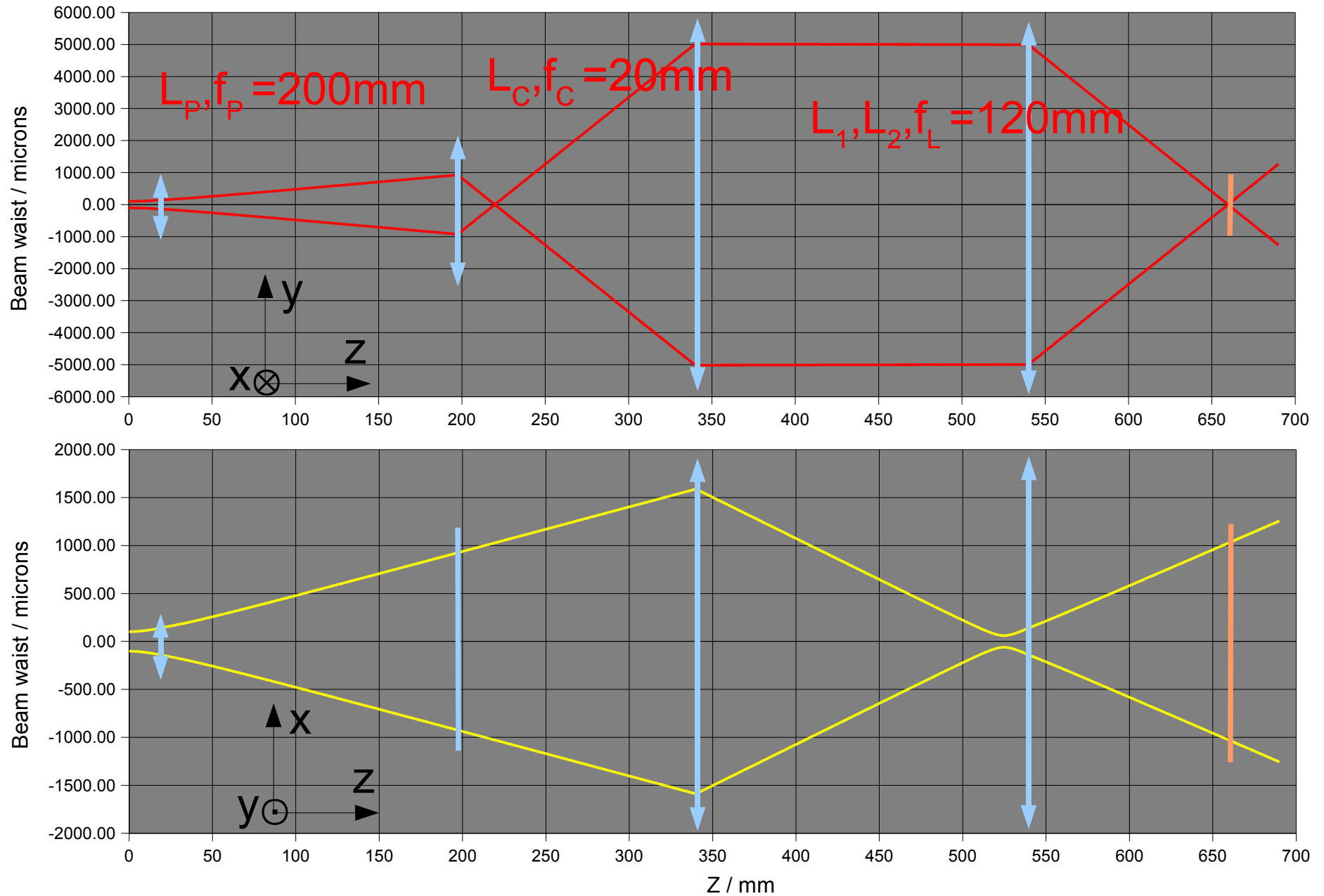


$f_p = 200\text{mm}$

Diffracted beam profile

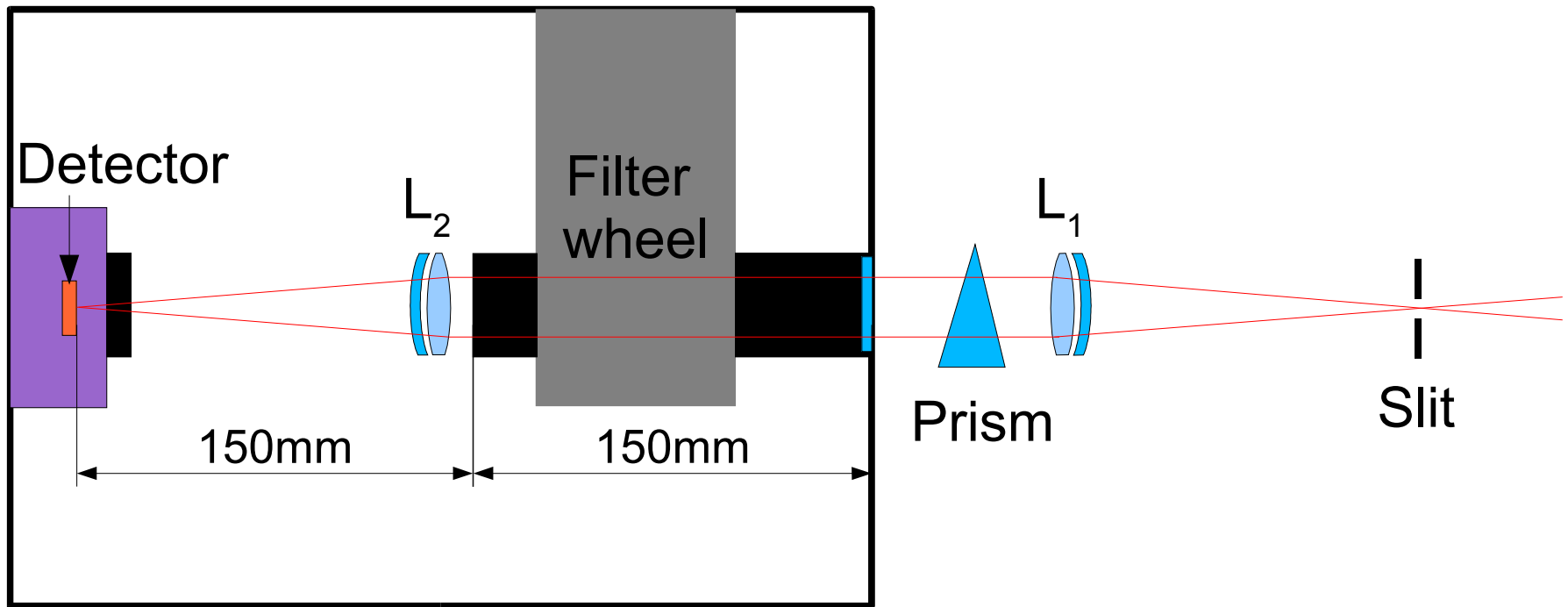


Diffracted beam profile



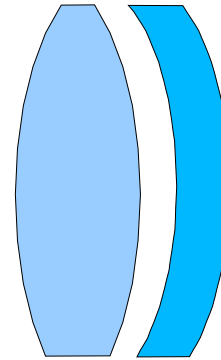
L_1 and L_2 doublets - 1

- Role: transport the dispersed image onto the detector
- L_1 , L_2 : same focal length
- L_2 in the detector dewar: $f_L = 100-120\text{mm}$

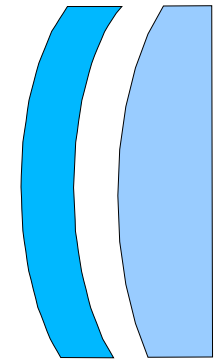


L_1 and L_2 doublets - 2

- Chosen design:
 - Air spaced Fraunhofer “crown” in front configuration



Crown Flint



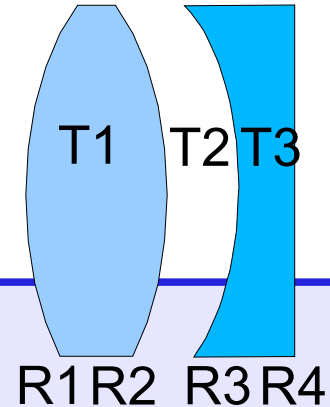
Flint Crown
Steinheil
configuration

Crown glass is one of the two principal types of optical glass, the other being *flint* glass. **Crown** glass is harder than *flint* glass, and has a lower index of refraction and lower dispersion.

- Selected glasses:
 - CaF_2 + *Fused Silica* (Keck design)
 - CaF_2 + *FTM16*

L_1 and L_2 doublets - 3

• Lens designed using zemax



1. Select a starting design:

$$R_1, R_2 = R_3 = -R_1, R_4 = \infty$$

2. Create a merit function controlling only the focal length

3. Use the optimisation routine to change R_1

4. Create the intermediate merit function which contains 4 operands controlling: the focal length, the longitudinal colour, the spherical aberration, and the coma.

5. Use the optimisation routine to change $R_1, R_2, R_3,$ and R_4

6. Create the final merit function and run the optimisation routine

L_1 and L_2 doublets - 4

Lens Data Editor

Edit Solves Options Help

Surf.	Type	Comment	Radius	Thickness	Glass	Semi-Diameter	Conic	Par 0 (unused)	Par 1 (unused)	Par 2 (unused)
OBJ	Standard		Infinity	Infinity		Infinity	0.000000			
STO	Standard		Infinity	100.000000		5.000000	0.000000			
2*	Standard	EDGE THICKNESS 2M..	69.235121	V	5.128400	E	CAF2	12.700000	U	0.000000
3*	Standard	EDGE THICKNESS 4M..	-42.256299	V	4.212222	E		12.700000	U	0.000000
4*	Standard		-38.317635	V	3.000000		FTM16	12.700000	U	0.000000
5*	Standard		-88.577678	V	108.676325	M		12.700000	U	0.000000
IMA	Standard		Infinity	-		6.289214	0.000000			

